

Normal Forms for Nonlinear Discrete Time Control Systems

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Abstract—We study the feedback classification of discrete-time control systems whose linear approximation around an equilibrium is controllable. We provide a normal form for systems under investigation.

I. INTRODUCTION

The method of normal forms has been a useful approach in studying the dynamical systems. This method, first introduced by Poincaré in his Ph.D. thesis (see [18]), has been successfully applied by the author to vector fields (differential dynamical systems) and maps (discrete-time systems), in order to provide a change of coordinates in which the system is in a “simplest” form (see also [1]).

For continuous-time control systems with controllable linearization, quadratic normal forms were obtained in [14] using change of coordinates and feedback. This result has been generalized to normal forms of any degree in [13]. Later on, normal forms for control systems with uncontrollable linearization has been derived [12], [16], [20], [22]. Quadratic and cubic normal forms for discrete-time control systems has been treated in [2], [6], [9], [17].

Although this method is formal, it has several applications in control theory. It has been used for the stabilization of systems with uncontrollable linearization, in continuous and discrete-time [4], [7], [5], [8], [10], [16], [17]. It has led to a complete description of symmetries around equilibrium [19], [26], and allowed the characterization of systems equivalent to feedforward forms [23], [24], [25].

In this paper, we propose a normal form, at any degree, for discrete-time control systems whose linearization is controllable.

The paper is organized as following: Section II deals with basic definitions. In Section III, we construct a normal form for discrete-time nonlinear control systems whose linear approximation is controllable. The proofs are given in Section IV.

II. Notations and definitions.

All objects, that is, functions, maps, vector fields, control systems, etc., are considered in a neighborhood of $0 \in \mathbb{R}^n$ and assumed to be C^∞ -smooth. For a smooth \mathbb{R} -valued function h , defined in a neighborhood of $0 \in \mathbb{R}^n$, we

denote by

$$h(x) = h^{[0]}(x) + h^{[1]}(x) + h^{[2]}(x) + \dots = \sum_{m=0}^{\infty} h^{[m]}(x)$$

its Taylor series expansion at $0 \in \mathbb{R}^n$, where $h^{[m]}(x)$ stands for a homogeneous polynomial of degree m .

Similarly, throughout the paper, for a map ϕ of an open subset of \mathbb{R}^n into \mathbb{R}^n (resp. for a vector field f on an open subset of \mathbb{R}^n), we will denote by $\phi^{[m]}$ (resp. by $f^{[m]}$) the term of degree m of its Taylor series expansion at $0 \in \mathbb{R}^n$, that is, each component $\phi_j^{[m]}$ of $\phi^{[m]}$ (resp. $f_j^{[m]}$ of $f^{[m]}$) is a homogeneous polynomial of degree m .

We consider the problem of transforming the discrete-time nonlinear control system

$$\Pi : x^+ = f(x, u), \quad x(\cdot) \in \mathbb{R}^n \quad u(\cdot) \in \mathbb{R},$$

where $x^+ = x(k+1)$, and $f(x, u) = f(x(k), u(k))$ for any $k \in \mathbb{N}$, by a feedback transformation of the form

$$\Upsilon : \begin{aligned} z &= \phi(x) \\ u &= \gamma(z, v) \end{aligned}$$

to a simpler form. The transformation Υ brings Π to the system

$$\tilde{\Pi} : z^+ = \tilde{f}(z, v),$$

whose dynamics are given by

$$\tilde{f}(z, v) = f(\phi^{-1}(z), \gamma(z, v)).$$

We suppose that $(0, 0) \in \mathbb{R}^n \times \mathbb{R}$ is an equilibrium point, that is, $f(0, 0) = 0$, and we denote by

$$\Pi^{[1]} : x^+ = Fx + Gu,$$

its linearization at this point, where

$$F = \frac{\partial f}{\partial x}(0, 0), \quad G = \frac{\partial f}{\partial u}(0, 0).$$

We will assume that this linearization is controllable, that is

$$\text{span} \{ F^i G : 0 \leq i \leq n-1 \} = \mathbb{R}^n.$$

Let us consider the Taylor series expansion Π^∞ of the system Π , given by

$$\Pi^\infty : x^+ = Fx + Gu + \sum_{m=2}^{\infty} f^{[m]}(x, u) \quad (1)$$

and the Taylor series expansion Υ^∞ of the feedback transformation Υ , given by

$$\Upsilon^\infty : \begin{aligned} z &= \phi(x) = Tx + \sum_{m=2}^{\infty} \phi^{[m]}(x) \\ u &= \gamma(x, v) = Kx + Lv + \sum_{m=2}^{\infty} \gamma^{[m]}(x, v) \end{aligned} \quad (2)$$

Throughout the paper, in particular in formulas (1) and (2), the homogeneity of $f^{[m]}$ and $\gamma^{[m]}$ will be taken with respect to the variables $(x, u)^t$ and $(x, v)^t$ respectively.

We first notice that, because of the controllability assumption, there always exists a linear feedback transformation

$$\Upsilon^1 : \begin{aligned} z &= Tx \\ u &= Kx + Lv \end{aligned}$$

bringing the linear part

$$\Pi^{[1]} : x^+ = Fx + Gu$$

into the Brunovsky canonical form (see [11])

$$\Pi_{CF}^{[1]} : z^+ = Az + Bv.$$

Then we study, successively for $m \geq 2$, the action of the homogeneous feedback transformations

$$\Upsilon^m : \begin{aligned} z &= x + \phi^{[m]}(x) \\ u &= v + \gamma^{[m]}(x, v) \end{aligned} \quad (3)$$

on the homogeneous systems

$$\Pi^{[m]} : x^+ = Ax + Bu + f^{[m]}(x, u). \quad (4)$$

Let us consider another homogeneous system

$$\tilde{\Pi}^{[m]} : z^+ = Az + Bv + \tilde{f}^{[m]}(z, v). \quad (5)$$

Definition 2.1: We say that the homogeneous system $\Pi^{[m]}$, given by (4), is feedback equivalent to the homogeneous system $\tilde{\Pi}^{[m]}$, given by (5), if there exist a homogeneous feedback transformation Υ^m , of the form (3), which brings the system $\Pi^{[m]}$ into the system $\tilde{\Pi}^{[m]}$ modulo higher order terms.

The starting point is the following proposition giving the equivalence conditions.

Proposition 2.1: The homogeneous feedback transformation Υ^m , defined by (3), brings the homogeneous system $\Pi^{[m]}$, given by (4), into the homogeneous system $\tilde{\Pi}^{[m]}$, given by (5), if and only if the following relation

$$\begin{aligned} \phi_j^{[m]}(Ax + Bu) - \phi_{j+1}^{[m]}(x) &= \tilde{f}_j^{[m]}(x, u) - f_j^{[m]}(x, u) \\ \phi_n^{[m]}(Ax + Bu) + \gamma^{[m]}(x) &= \tilde{f}_n^{[m]}(x, u) - f_n^{[m]}(x, u) \end{aligned}$$

hold for all $1 \leq j \leq n-1$.

III. MAIN RESULTS.

In this section we will establish our main results. Let us denote the control by $v = z_{n+1}$, and for any $1 \leq i \leq n+1$,

$$\tilde{z}_i = (z_1, \dots, z_i).$$

Our main result for discrete-time nonlinear control systems with controllable linearization is as following.

Theorem 3.1: The control system Π^∞ , defined by (1), is feedback equivalent, by a formal feedback transformation Υ^∞ of the form (2), to the normal form

$$\Pi_{NF}^\infty : z^+ = Az + Bv + \sum_{m=2}^{\infty} \tilde{f}^{[m]}(z, v),$$

where for any $m \geq 2$, we have

$$\tilde{f}_j^{[m]}(z, v) = \begin{cases} \sum_{i=j+2}^{n+1} z_i P_{j,i}^{[m-2]}(\tilde{z}_i) & \text{if } 1 \leq j \leq n-1 \\ 0 & \text{if } j = n. \end{cases} \quad (6)$$

As the homogeneous feedback transformations Υ^m leave invariant the terms of degree less than m , Theorem 3.1 follows from a successive application of Theorem 3.2 below.

Theorem 3.2: The homogeneous control system $\Pi^{[m]}$, defined by (4), is feedback equivalent, by a homogeneous feedback transformation Υ^m of the form (3), to the normal form

$$\Pi_{NF}^{[m]} : z^+ = Az + Bv + \tilde{f}^{[m]}(z, v),$$

where for any $m \geq 2$, the vector field $\tilde{f}^{[m]}(z, v)$ is given by (6).

A. Example

Consider the Bressan and Rampazzo pendulum (see [3], [21]) described by the equations

$$\begin{aligned} \dot{x}_1 &= x_2 \\ \dot{x}_2 &= -g \sin x_3 + x_1 x_4^2 \\ \dot{x}_3 &= x_4 \\ \dot{x}_4 &= u, \end{aligned}$$

where x_1 denotes the length of the pendulum, x_2 its velocity, x_3 the angle of the pendulum with respect to the horizontal, x_4 its angular velocity, and g the gravity constant.

We discretize the system by taking

$$\begin{aligned} \hat{x}_1 &= x_1^+ - x_1, & \hat{x}_2 &= x_2^+ - x_2, \\ \hat{x}_3 &= x_3^+ - x_3, & \hat{x}_4 &= x_4^+ - x_4. \end{aligned}$$

The system above rewrites

$$\begin{aligned} x_1^+ &= x_1 + x_2 \\ x_2^+ &= x_2 - g \sin x_3 + x_1 x_4^2 \\ x_3^+ &= x_3 + x_4 \\ x_4^+ &= x_4 + u. \end{aligned}$$

Let us consider the change of coordinates

$$\begin{aligned} z_1 &= x_1 \\ z_2 &= x_2 + x_1 \\ z_3 &= -g \sin x_3 + 2x_2 + x_1 \\ z_4 &= -g \sin(x_4 + x_3) + 3x_2 - 2g \sin x_3 + 2x_1 x_4^2 + x_1 \\ v &= z_4^+ \end{aligned}$$

whose inverse is such that $x_4 = h(z_1, z_2, z_3, z_4)$ is a smooth function. This change of coordinates takes the system into

the form

$$\begin{aligned} z_1^+ &= z_2 \\ z_2^+ &= z_3 + z_1 h^2(z_1, z_2, z_3, z_4) \\ z_3^+ &= z_4 \\ z_4^+ &= v. \end{aligned}$$

Actually the function $h^2(z_1, z_2, z_3, z_4)$ could be decomposed as

$$h^2(z_1, z_2, z_3, z_4) = h_1(z_1, z_2, z_3) + z_4 h_2(z_1, z_2, z_3, z_4)$$

where the 1-jet at 0 of h_1 is zero and $h_2(0) = 0$. Put $H_1(z_1, z_2, z_3) = z_1 h_1(z_1, z_2, z_3)$.

The objective is to show that we can get rid of the terms $H_1(z_1, z_2, z_3)$. Let us suppose that the k -jet at 0 of H_1 is zero.

Consider the change of coordinates $\tilde{z}_1 = z_1, \tilde{z}_2 = z_2, \tilde{z}_3 = z_3 + H_1(z_1, z_2, z_3), \tilde{z}_4 = z_4^+$. This change of coordinates, completed by the feedback $\tilde{z}_4^+ = w$, takes the system into the form

$$\begin{aligned} \tilde{z}_1^+ &= \tilde{z}_2 \\ \tilde{z}_2^+ &= \tilde{z}_3 + \tilde{H}_1(\tilde{z}_1, \tilde{z}_2, \tilde{z}_3) + \tilde{z}_1 \tilde{z}_4 \tilde{H}_2(\tilde{z}_1, \tilde{z}_2, \tilde{z}_3, \tilde{z}_4) \\ \tilde{z}_3^+ &= \tilde{z}_4 \\ \tilde{z}_4^+ &= w, \end{aligned}$$

where $\tilde{H}_1(\tilde{z}_1, \tilde{z}_2, \tilde{z}_3)$ and $\tilde{H}_2(\tilde{z}_1, \tilde{z}_2, \tilde{z}_3, \tilde{z}_4)$ are some smooth functions. It is enough to remark that the $(k+2)$ -jet at 0 of $\tilde{H}_1(\tilde{z}_1, \tilde{z}_2, \tilde{z}_3)$ is zero because the 2-jet of $z_1 z_4 H_2(z)$ is zero. Then by iteration we can cancel terms $H_1(z_1, z_2, z_3)$ and put the system into the desired normal form

$$\begin{aligned} z_1^+ &= z_2 \\ z_2^+ &= z_3 + z_1 z_4 H(z_1, z_2, z_3, z_4) \\ z_3^+ &= z_4 \\ z_4^+ &= v. \end{aligned}$$

IV. PROOFS

In this section we will prove our main result. Before let us state the following useful lemma.

Lemma 4.1: If $h^{[m]}(z, u) = h^{[m]}(z_2, \dots, z_n, u)$ is a homogeneous polynomial depending exclusively on the variables z_2, \dots, z_n and the control u , then there is a unique homogeneous polynomial $H^{[m]}(z) = H^{[m]}(z_1, \dots, z_n)$ such that $H^{[m]}(Az + Bu) = h^{[m]}(z, u)$.

The proof of this lemma is straightforward, and hence will be omitted.

A. Proof of Theorem 3.2

The proof will be constructive and based on an inductive argument. Let us consider the system $\Pi^{[m]}$ given by

$$\begin{aligned} x_1^+ &= x_2 + f_1^{[m]}(x, u) \\ &\dots \\ x_{n-1}^+ &= x_n + f_{n-1}^{[m]}(x, u) \\ x_n^+ &= u + f_n^{[m]}(x, u). \end{aligned} \quad (7)$$

Applying the feedback $v = u + f_n^{[m]}(x, u)$, we can annihilate the terms $f_n^{[m]}(x, u)$, and hence we can assume that $f_n^{[m]}(x, u) = 0$.

Let us suppose that for some $1 \leq j \leq n-1$, the system (7) has been taken to the form

$$\begin{aligned} x_1^+ &= x_2 + f_1^{[m]}(x, u) \\ &\dots \\ x_j^+ &= x_{j+1} + f_j^{[m]}(x, u) \\ x_{j+1}^+ &= x_{j+2} + \bar{f}_{j+1}^{[m]}(x, u) \\ &\dots \\ x_{n-1}^+ &= x_n + \bar{f}_{n-1}^{[m]}(x, u) \\ x_n^+ &= u, \end{aligned} \quad (8)$$

where for any $j+1 \leq l \leq n-1$, we have

$$\bar{f}_l^{[m]}(x, u) = \sum_{i=l+2}^{n+1} x_1 x_i P_{l,i}^{[m-2]}(\bar{x}_i).$$

We first decompose the component $f_j^{[m]}(x, u)$ uniquely as follows

$$\begin{aligned} f_j^{[m]}(x, u) &= \sum_{i=j+2}^{n+1} x_1 x_i P_{j,i}^{[m-2]}(\bar{x}_i) \\ &+ \sum_{i=1}^{j+1} x_1 x_i P_{j,i}^{[m-2]}(\bar{x}_i) + R_j^{[m]}(x_2, \dots, x_n, u). \end{aligned}$$

We consider the feedback transformation

$$\Upsilon^m : \begin{aligned} z &= x + \phi^{[m]}(x) \\ u &= v + \gamma^{[m]}(x, v) \end{aligned}$$

whose components $\phi_1^{[m]}(x), \dots, \phi_n^{[m]}(x)$, and $\gamma^{[m]}(x, v)$ are defined as following.

Using Lemma 4.1, we define $\phi_j^{[m]}(x)$ such that

$$\phi_j^{[m]}(Ax + Bu) = -R_j^{[m]}(x_2, \dots, x_n, u) \quad (9)$$

and we take

$$\begin{aligned} \phi_{j+1}^{[m]}(x) &= \sum_{i=1}^{j+1} x_1 x_i P_{j,i}^{[m-2]}(\bar{x}_i) \\ \phi_{j+2}^{[m]}(x) &= \phi_{j+1}^{[m]}(Ax + Bu) \\ &\dots \\ \phi_n^{[m]}(x) &= \phi_{n-1}^{[m]}(Ax + Bu) \\ \gamma^{[m]}(x) &= \phi_n^{[m]}(Ax + Bu). \end{aligned} \quad (10)$$

The components $\phi_1^{[m]}(x), \dots, \phi_{j-1}^{[m]}(x)$ could be taken to be zero or arbitrary. Moreover, we can notice that the components $\phi_j^{[m]}(x), \dots, \phi_n^{[m]}(x)$ did not depend on the control u . Actually, for any $j \leq l \leq n$, we have

$$\phi_l^{[m]}(x) = \phi_l^{[m]}(x_1, \dots, x_l).$$

Applying Proposition 2.1, we easily deduce that the transformation Υ^m whose components are given by (9)-(10) takes the system (8) into the form

$$\begin{aligned} z_1^+ &= z_2 + f_1^{[m]}(z, u) \\ &\dots \\ z_{j-1}^+ &= z_j + f_{j-1}^{[m]}(z, u) \\ z_j^+ &= z_{j+1} + \bar{f}_j^{[m]}(z, u) \\ &\dots \\ z_{n-1}^+ &= z_n + \bar{f}_{n-1}^{[m]}(z, u) \\ z_n^+ &= u, \end{aligned}$$

where for any $j \leq l \leq n - 1$, we have

$$\bar{f}_l^{[m]}(z, u) = \sum_{i=l+2}^{n+1} z_1 z_i P_{l,i}^{[m-2]}(\bar{z}_i). \quad (11)$$

This achieves the proof of Theorem 3.2.

V. REFERENCES

- [1] Arnold, V. I. (1983). *Geometrical Methods in the Theory of Ordinary Differential Equations*, Springer Verlag.
- [2] Barbot, J.-P., S. Monaco and D. Normand-Cyrot (1997). Quadratic forms and approximative feedback linearization in Discrete Time, *International Journal of Control*, **67**, 567-586.
- [3] Bressan, A. and Rampazzo, F. *On differential systems with quadratic impulses and their applications to Lagrangian mechanics*, in *SIAM Journal on Control and Optimization*, **31**, (1993) pp. 1205-1230.
- [4] Hamzi, B., J.-P. Barbot and W. Kang (1998). Bifurcation and Topology of Equilibrium Sets for Nonlinear Discrete-Time Control Systems, *Proc. of the Nonlinear Control Systems Design Symposium (NOLCOS'98)*, pp. 35-38.
- [5] Hamzi, B., J.-P. Barbot and W. Kang (1999). "Stabilization of Nonlinear Discrete-Time Control Systems with Uncontrollable Linearization". In *Modern Applied Mathematics Techniques in Circuits, Systems and Control*", *World Scientific and Engineering Society Press*, pp. 278-283. Also in *Proc. of the 3rd IEEE/MACS Multiconference on Circuits, Systems, Communications and Computers*, pp. 4581-4586.
- [6] Hamzi, B., J.-P. Barbot and W. Kang (1999). Normal forms for discrete time parameterized systems with uncontrollable linearization, *Proceedings of the 38th IEEE Conference on Decision and Control*, vol. 2, pp. 2035-2038.
- [7] Hamzi, B., J.-P. Barbot and W. Kang (1999). Bifurcation for discrete-time parameterized systems with uncontrollable linearization, *Proc. of the 38th IEEE Conference on Decision and Control*, vol.1, pp. 684-688.
- [8] Hamzi, B. (2001). *Analyse et commande des systèmes non linéaires non commandables en première approximation dans le cadre de la théorie des bifurcations*, Ph.D. Thesis, University of Paris XI-Orsay, France.
- [9] Hamzi, B., J.-P. Barbot, S. Monaco, and D. Normand-Cyrot (2001). Normal Forms versus Naimark-Sacker Bifurcation Control, invited paper to the *Nonlinear Control Systems Design Symposium (NOLCOS'01)*.
- [10] Hamzi, B., J.-P. Barbot, S. Monaco, and D. Normand-Cyrot (2001). Nonlinear Discrete-Time Control of Systems with a Naimark-Sacker Bifurcation, *Systems and Control Letters*, **44**, 245-258.
- [11] Kailath, T. (1980). *Linear Systems*. Prentice-Hall.
- [12] Kang, W. (1995). Quadratic normal forms of nonlinear control systems with uncontrollable linearization, *Proceedings of the 34th IEEE Conference on Decision and Control*, vol. 1, pp. 608-612.
- [13] Kang, W. (1996a). Extended Controller Form and Invariants of Nonlinear Control Systems with a Single Input. *Journal of Mathematical Systems, Estimation, and Control*, **6**, 27-51.
- [14] Kang, W. and A.J. Krener (1992). Extended quadratic controller normal form and dynamic state feedback linearization of nonlinear systems, *Siam J. Control and Optimization*, **30**, 1319-1337.
- [15] Krener, A. J. (1984). Approximate linearization by state feedback and coordinate change, *Systems and Control Letters*, **5**, 181-185.
- [16] Krener, A.J., W. Kang, and D.E. Chang (2001), Control Bifurcations, submitted to *IEEE trans. on Automatic Control*.
- [17] Krener, A.J. and L. Li (2002). Normal Forms and Bifurcations of Discrete Time Nonlinear Control Systems, *SIAM J. on Control and Optimization*, **40**, 1697-1723.
- [18] Poincaré, H. (1929). Sur les propriétés des fonctions définies par les équations aux différences partielles. *Oeuvres*, pp. XCIX-CX, Gauthier-Villars: Paris.
- [19] W. Respondek and I. A. Tall, How Many Symmetries Does Admit a Nonlinear Single-Input Control System around Equilibrium, in *Proc. of the 40th CDC*, pp. 1795-1800, Florida, (2001).
- [20] I. A. Tall, Classification par bouclage des systèmes de contrôles non linéaires mono-entrée: formes normales, formes canoniques, invariants et symétries. Ph. D. Thesis, INSA de Rouen, (2000).
- [21] I. A. Tall and W. Respondek, Feedback classification of nonlinear single-input control systems with controllable linearization: normal forms, canonical forms, and invariants, in *SIAM Journal on Control and Optimization*, pp. 1498-1531, 2002.
- [22] I. A. Tall and W. Respondek, Normal forms and invariants of nonlinear single-input systems with noncontrollable linearization, *NOLCOS'01*, Petersburg, Russia, (2001).
- [23] I. A. Tall and W. Respondek, Feedback Equivalence to a Strict Feedforward Form for Nonlinear Single-Input Systems, to appear in *International Journal of Control*.
- [24] I. A. Tall and W. Respondek, Transforming a Single-Input Nonlinear System to a Strict Feedforward Form via Feedback, *Nonlinear Control in the Year 2000*, A. Isidori, F. Lamnabhi, and W. Respondek, (eds.), Springer-Verlag, **2**, pp. 527-542, London, England, (2001).
- [25] I. A. Tall and W. Respondek, Feedback Equivalence to Feedforward Form for Nonlinear Single-Input Systems, *Dynamics, Bifurcations and Control*, F. Colonius and L. Grune (eds.), *LNCS*, **273**, pp. 269-286, Springer-Verlag, Berlin Heidelberg, (2002).

- [26] I. A. Tall and W. Respondek, Nonlinearizable Analytic Single-Input Control Systems with Controllable Linearization DO Not Admit Stationary Symmetries, *Systems and Control Letters*, 46 (1), pp. 1-16, (2002).